

EN 1990: Basis of Structural Design

EN 1991: Action on structures

Example

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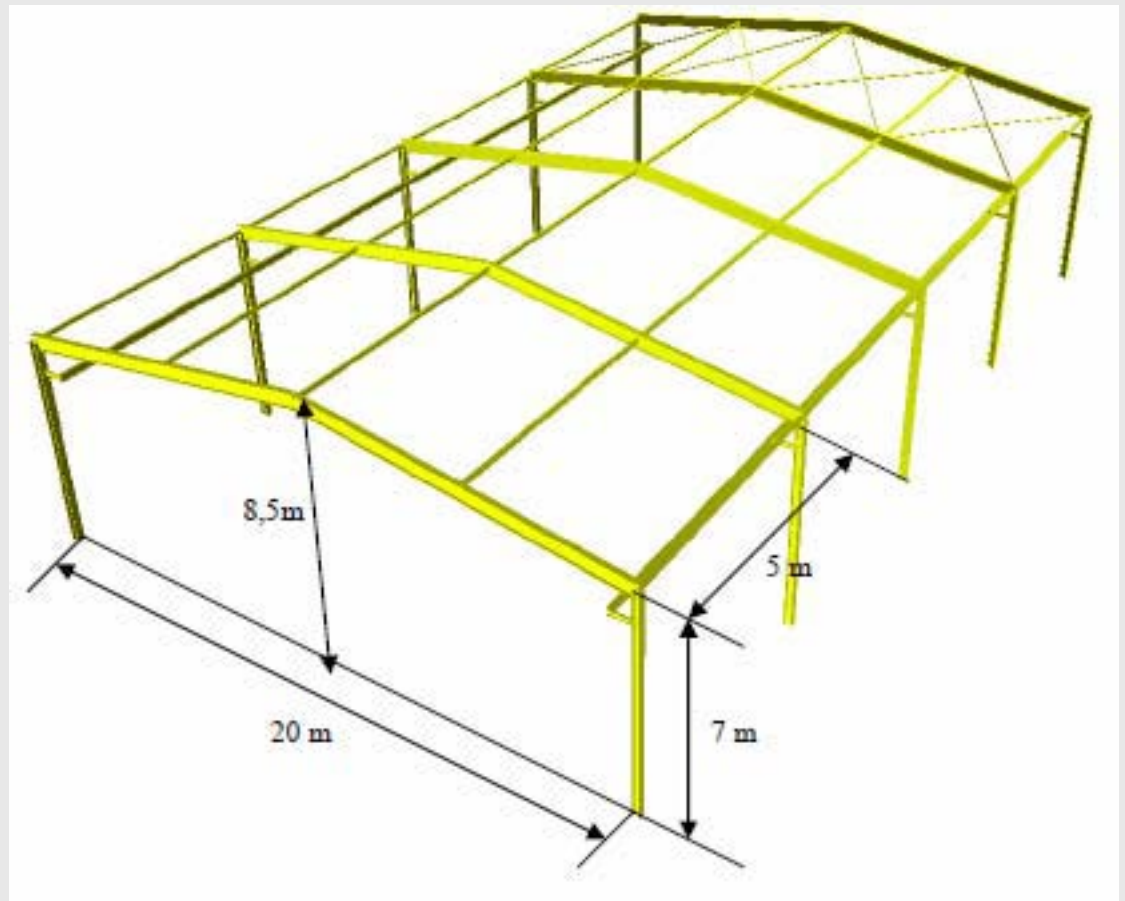
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Structural system of the building

- single storey industrial hall
- 20 m wide, 20 m long
- 5 single bay portal frames
- columns 7 m height, 8,5 m at roof ridge
- crane runway girders at 6m height
- columns HEA 400, beams IPE 550, crane girders I 60, consoles I 280, wind bracing H 60x60x6
- construction steel S 235



Definition of the characteristic values

1. Permanent actions

1.1 Self weight of structural members:

γ : the mean value of the specific weight of steel,
78,5 kN/m³ (EN 1991-1-1, Appendix A).

the distributed self weight
per unit length of members:

$$g_k = \gamma A,$$

A is the cross-sectional area

1.2 Roof and wall cladding

distributed load $h = 0,3 \text{ kN/m}^2$

Line load due to self weight

$$g_{\text{roof}} = g_{\text{wall}} = 5 \text{ m} \times 0,3 \text{ kN/m}^2 \\ = 1,5 \text{ kN/m}$$

Element	Section	g_k [kN/m]
portal column	HEA 400	1,25
portal beam	IPE 550	1,05
purlin	HEA 200	0,42
crane girder	I 280	0,42
console	I 280	0,48
wind bracing	H 60x60x6	0,05

Definition of the characteristic values (cont.-d)

2. Imposed loads

2.1 Imposed loads on roofs

For roof category H 'roof not accessible except for normal maintenance and repair' (EN 1991-1-1, Table 6.9) the distributed and concentrated loads are

$$q_k = 0,4 \text{ kN/m}^2, Q_k = 1,0 \text{ kN}$$

$$p_{\text{roof}} = 5 \text{ m} \times 0,4 \text{ kN/m}^2 = 2,0 \text{ kN/m on the girder}$$



2.2 Actions imposed by the crane

$P_{\text{max}} = 180 \text{ kN}$, $P_{\text{min}} = 60 \text{ kN}$ including dynamic effects.

Horizontal force due to the movement of the crane: $H_x = 0,1 P$.

Position of the crane: the centerline between the wheels is in the plane of the frame.

Definition of the characteristic values (cont.-d)

2.3 Snow load

2.3.1 The characteristic value of ground snow load $s_k = 1,88 \text{ kN/m}^2$

2.3.2 The exposure coefficient $C_e = 1,0$ (*'wind swept' or 'sheltered' conditions do not apply*)

2.3.3 Thermal coefficient $C_t = 1,0$ (*normal thermal roof insulation is assumed*)

2.3.4 The snow load shape coefficients μ depend on the roof angle α

For 'dupitched' roof with $\alpha = 8,5^\circ$: $\mu_1 = \mu_2 = 0,8$.

2.3.5 The snow load s_{roof}

$$s_{roof} = \mu_1 \times C_e \times C_t \times s_k = 0,8 \times 1,0 \times 1,0 \times 1,88 = 1,5 \text{ kN/m}^2$$

and the snow load s on the girder

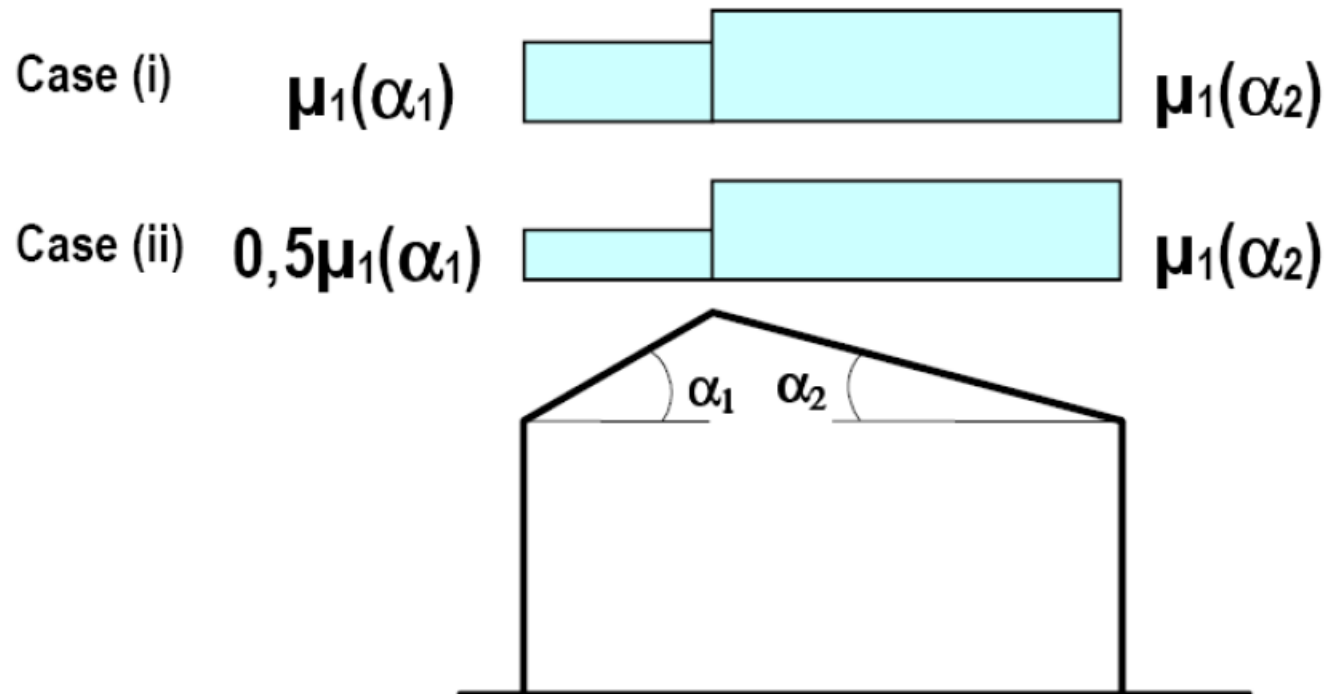
$$s = s_{roof} \times W = 1,5 \times 5 = 7,5 \text{ kN/m}$$

2.3.6 Two snow load arrangements

are considered (according to EN 1991-1-3)

Definition of the characteristic values (cont.-d)

2.3 Snow load (cont.-d)



Definition of the characteristic values (cont.-d)

2.4 Wind load

2.4.1 Fundamental basic wind velocity $v_{b,0} = 25 \text{ m/s}$ (wind map, national annex to EN 1991-1-4).

2.4.2 Basic wind velocity v_b (with usual values for directional and seasonal factors) :

$$V_b = v_{b,0} \cdot c_{dir} \cdot c_{sea} = 25 \cdot 1,0 \cdot 1,0 = 25 \text{ m/s}$$

2.4.3 Mean wind velocity $v_m(z)$ at reference height $z_e = 8,5 \text{ m}$

$$v_m(z) = c_r(z) \cdot c_o(z) \cdot v_b = 18,4 \text{ m/s}$$

with orography factor $c_o(z) = 1$, roughness factor $c_r(z) = k_r \cdot \ln(z/z_0)$
terrain category III (suburban or industrial areas): $I_v = 0,22$, $z_0 = 0,3$

2.4.4 Peak velocity pressure $q_p(z)$

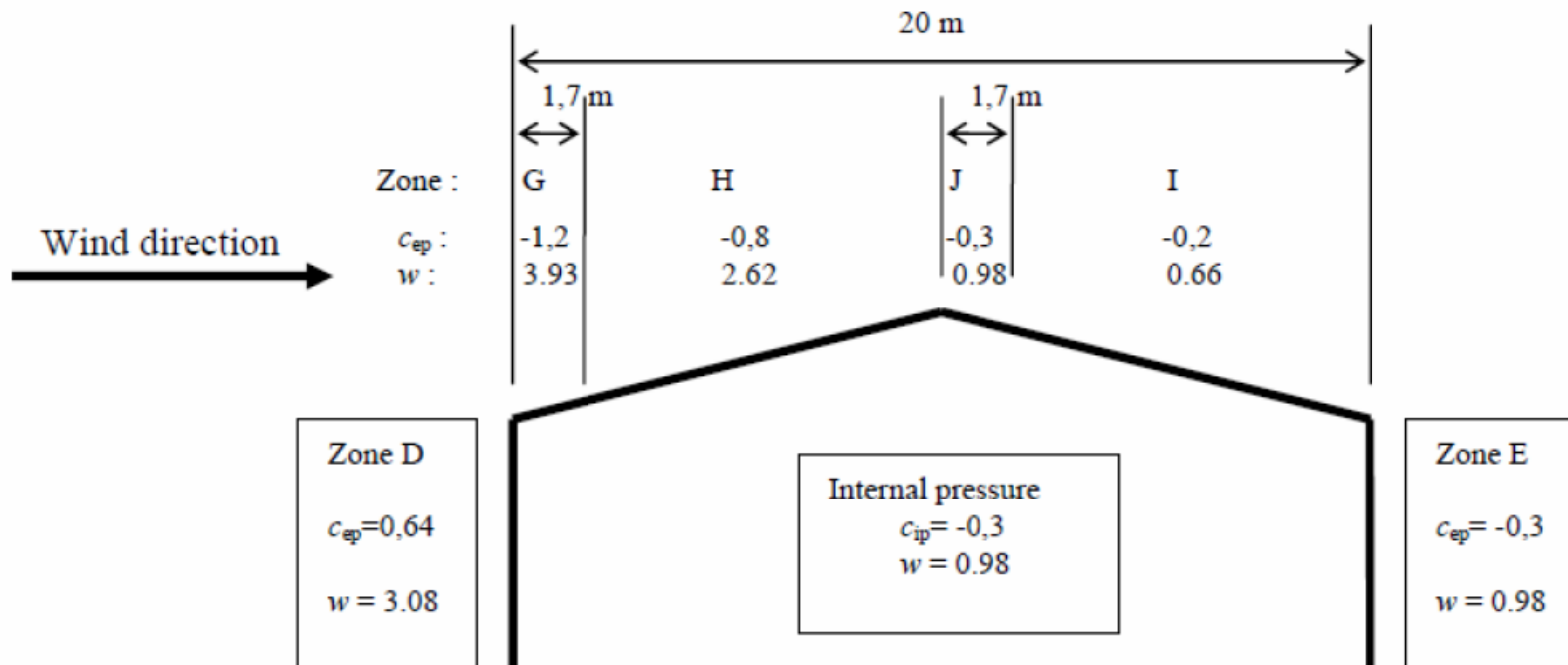
$$q_p(z) = \{1 + 7 I_v / [c_o(z) \ln(z/z_0)]\} \frac{1}{2} \rho v_m(z) = 0,655 \text{ kN/m}^2$$

with air density $\rho = 1,25 \text{ kg/m}^3$ and turbulence intensity $I_v = 1,0$

2.4.5 External c_{pe} and internal c_{pi} wind pressure coefficients and wind load w : $w = (c_{pe} - c_{pi}) q_p$

Definition of the characteristic values (cont.-d)

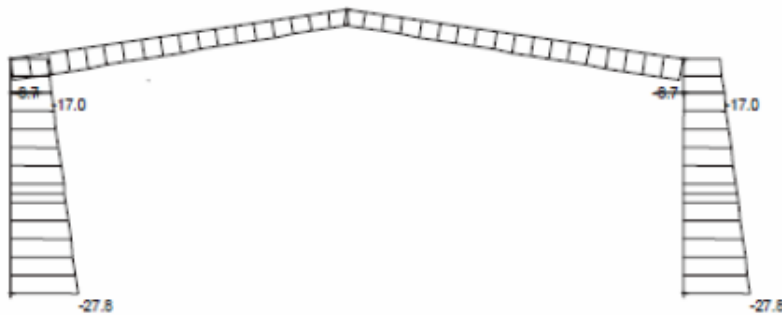
2.3 Wind load (cont.-d)



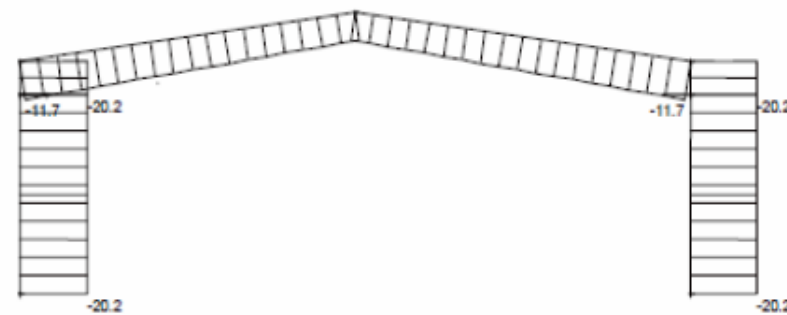
Internal forces due to actions

Internal axial forces:

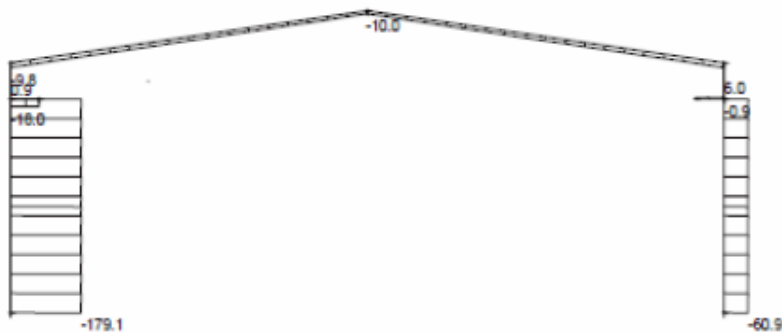
Self weight, roof and wall cladding



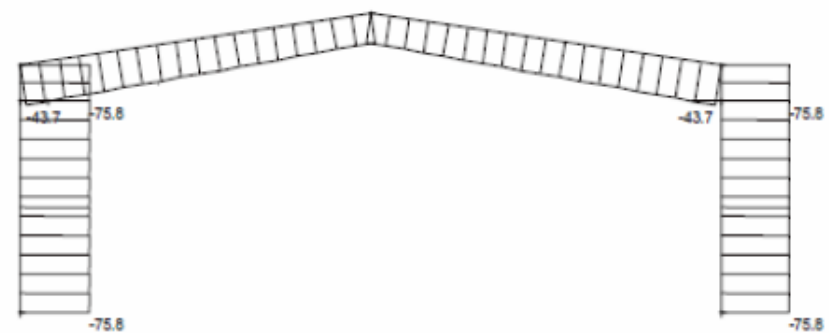
Imposed load: roof, wall



Crane: vertical load and horizontal side load



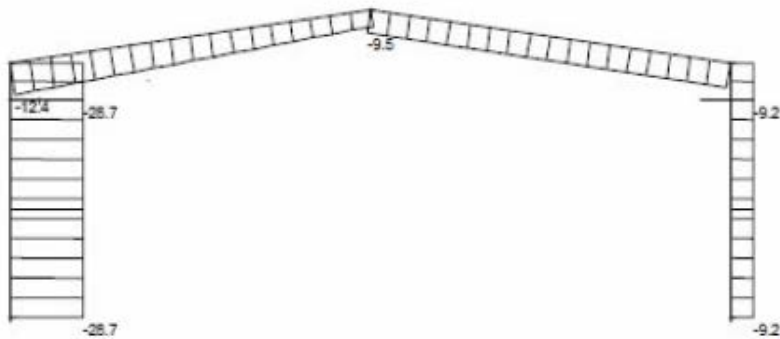
Snow load, case I



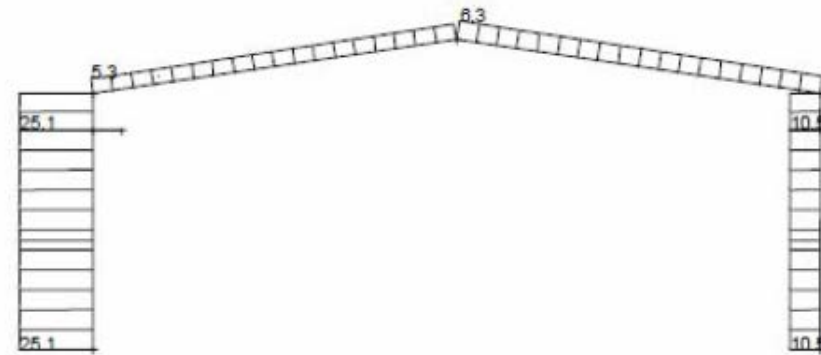
Internal forces due to actions (cont.-d)

Axial forces (cont'd):

Snow load, case II

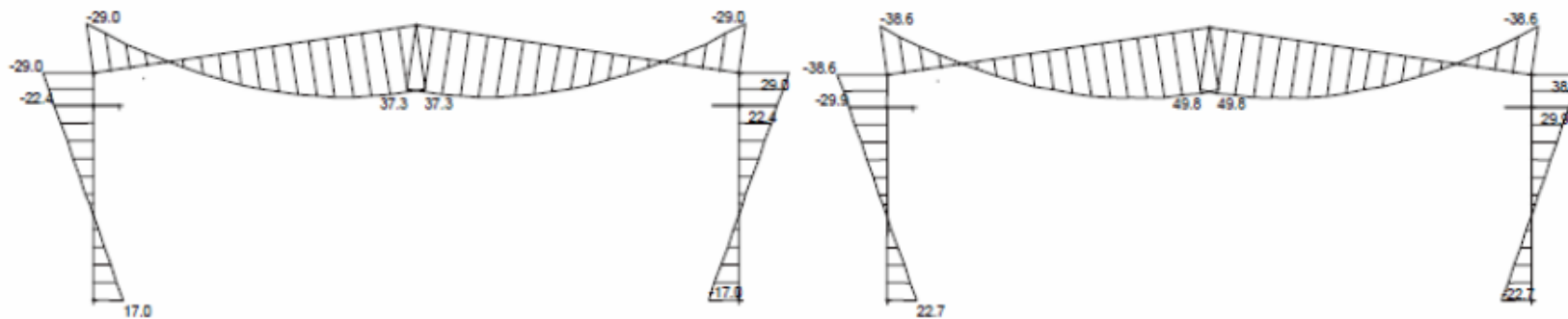


Wind load



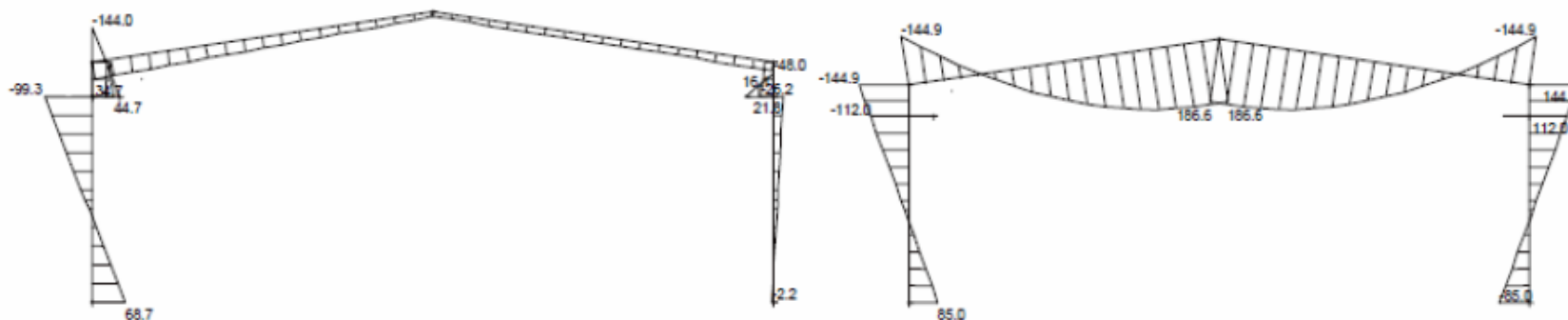
Internal forces due to actions (cont.-d)

Bending moments:



Crane: vertical load and horizontal side load

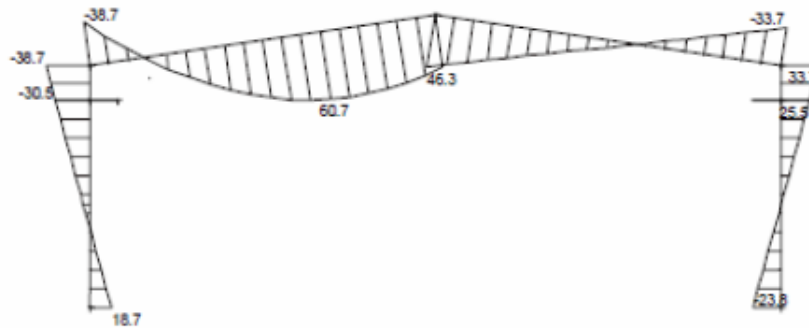
Snow load, case I



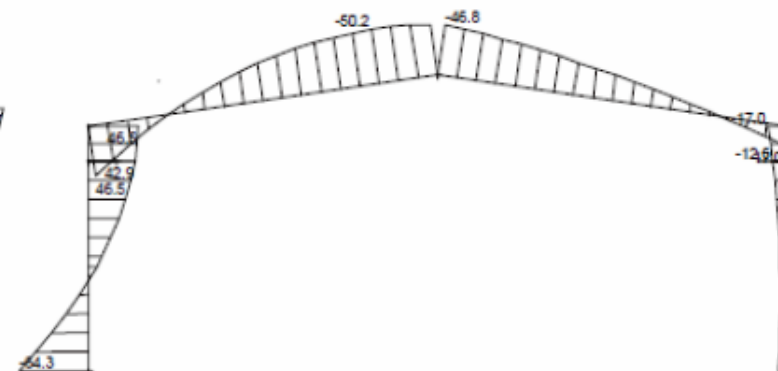
Internal forces due to actions (cont.-d)

Bending moments (cont'd):

Snow load, case II



Wind load



Combination of actions

Load cases overview

Loading	COLUMN				BEAM			
	Start point		End point		Start point		End point	
	N [kN]	M [kNm]	N [kN]	M [kNm]	N [kN]	M [kNm]	N [kN]	M [kNm]
self weight	-27,8	17,0	-17,0	-29,0	-8,7	-29,0	-8,0	37,3
roof	-20,2	22,7	-20,2	-38,6	-20,2	-38,6	-8,0	49,8
crane	-179,1	68,7	-9,8	-99,3	-10,0	34,7	-10,0	10,0
snow I	-75,8	85,0	-75,8	-144,9	-43,7	-144,9	-30,0	186,6
snow II	-28,7	18,7	-28,7	-38,7	-12,4	-38,7	-9,5	46,3
wind	-10,5	-12,6	-10,5	-17,0	5,3	17,0	5,3	-46,8

Combination of actions (cont.-d)

Ultimate limit state, fundamental combinations:

The design value of the effects of actions E_d is calculated from the combination of actions according to the expression (6.10) of the EN 1990

$$E_d = E(\gamma_{G,j} G_{k,j} + \gamma_{Q,1} Q_{k,1} + \sum \gamma_{Q,i} \psi_{0,i} Q_{k,i})$$

Combination I, leading action R: $1,35 \cdot G + 1,5 \cdot (R + 0,7 \cdot C + 0,5 \cdot S + 0,6 \cdot W)$

Combination II, leading action C: $1,35 \cdot G + 1,5 \cdot (C + 0,0 \cdot R + 0,5 \cdot S + 0,6 \cdot W)$

Combination III, leading action S: $1,35 \cdot G + 1,5 \cdot (S + 0,0 \cdot R + 0,7 \cdot C + 0,6 \cdot W)$

Combination IV, leading action W: $1,35 \cdot G + 1,5 \cdot (W + 0,0 \cdot R + 0,7 \cdot C + 0,5 \cdot S)$

where: G - self weight; R - imposed load on roofs; C - crane load;
S - snow load, case I; W – wind load.

Combination of actions (cont.-d)

$$E_d = E\{\gamma_{G,j}G_{k,j}; \gamma_P P; \gamma_{Q,1}Q_{k,1}; \gamma_{Q,i}\psi_{0,i}Q_{k,i}\} \quad j \geq 1; i > 1$$

$$\leq R_d = \frac{1}{\gamma_{Rd}} R\{X_{d,i}; a_d\} = \frac{1}{\gamma_{Rd}} R\left\{\eta_i \frac{X_{k,i}}{\gamma_{m,i}}; a_d\right\} \quad i \geq 1$$